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## TITLE OF THE INVENTION

APPARATUS AND METHOD FOR SYMBOL ALIGNMENT IN A  
MULTI-POINT OFDM/DMT DIGITAL COMMUNICATIONS SYSTEM

## CROSS-REFERENCE TO RELATED APPLICATIONS

The present application is a continuation-in-part application of U.S.S.N.  
08/700,779, filed August 22, 1996.

## STATEMENT REGARDING FEDERALLY SPONSORED RESEARCH OR DEVELOPMENT

Not Applicable

## BACKGROUND OF THE INVENTION

The present invention is directed to an OFDM/DMT digital communications system. More particularly, the present invention is directed to an apparatus and method for attaining symbol alignment in a multi-point, OFDM/DMT digital communications system.

Multi-point communications systems having a primary site that is coupled for communication with a plurality of secondary sites are known. One such communications system type is a cable telephony system. Cable telephony systems transmit and receive telephone call communications over the same cable transmission media as used to receive cable television signals and other cable services.

One cable telephony system currently deployed and in commercial use is

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the Cablesan 2300 system available from Tellabs, Inc. The Cablesan 2300 system uses a head end unit that includes a primary transmitter and primary receiver disposed at a primary site. The head end unit transmits and receives telephony data to and from a plurality of remote service units that are located at respective secondary sites. This communication scheme uses TDM QPSK modulation for the data communications and can accommodate approximately thirty phone calls within the 1.9 MHz bandwidth typically allocated for such communications.

As the number of cable telephony subscribers increases over time, the increased use will strain the limited bandwidth allocated to the cable telephony system. Generally stated, there are two potential solutions to this bandwidth allocation problem that may be used separately or in conjunction with one another. First, the bandwidth allocated to cable telephony communications may be increased. Second, the available bandwidth may be used more efficiently. It is often impractical to increase the bandwidth allocated to the cable telephony system given the competition between services for the total bandwidth available to the cable service provider. Therefore, it is preferable to use the allocated bandwidth in a more efficient manner. One way in which the assigned bandwidth may be used more efficiently is to use a modulation scheme that is capable of transmitting more information within a given bandwidth than the TDM QPSK modulation scheme presently employed.

The present inventors have recognized that OFDM/DMT modulation schemes may provide such an increase in transmitted information for a given

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## BRIEF SUMMARY OF THE INVENTION

A multi-point communications system is set forth herein. The communications system comprises a head end unit disposed at a primary site and a plurality of receivers disposed at remote sites. The head end unit includes a transmitter for transmitting OFDM/DMT symbols over a predetermined number of bins across a transmission medium. The OFDM/DMT symbols are respectively transmitted in periodically occurring formatted symbol frames. The cyclic prefix includes a predetermined periodic signal superimposed thereon. The receivers receive the OFDM/DMT symbols over a subset of the predetermined number of bins from the transmission medium and use the superimposed signals to attain symbol alignment. Preferably, the superimposed signal is an impulse signal that varies in polarity throughout the transmission cycle and which is superimposed on one or more symbols occurring during a cyclic prefix of the formatted symbol frames.

In accordance with a further aspect of the present invention, the receivers apply a predetermined incremental phase shift to received samples corresponding to the received OFDM/DMT symbols to thereby compensate for phase shifts resulting from the cyclic prefix.

The multi-point communications system may include a similar system for aligning symbols transmissions from a remote service unit having a transmitter. Such a system includes a plurality of remote service units each including a transmitter for transmitting OFDM/DMT symbols over a predetermined number of bins across a transmission medium. Each of the

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plurality of remote service units is operable in a symbol alignment mode in which the transmitter transmits a broad band periodic signal. The head end unit includes a receiver for receiving the OFDM/DMT symbols, including the broad band periodic signal, from the transmission medium. The head end unit uses the time position of the broad band periodic signal to align the symbol transmissions of the remote service unit with other ones of the remote service units.

Other features and advantages of the present invention will become apparent upon review of the following detailed description and accompanying drawings.

BRIEF DESCRIPTION OF THE SEVERAL  
VIEWS OF THE DRAWINGS

FIG. 1 is a schematic block diagram of a multi-point communications system having a plurality of remote service units disposed at a plurality of secondary sites wherein each of the remote service units comprises a receiver having an improved receiver architecture.

FIG. 2 is a block diagram of illustrative embodiments of the head end unit and a remote service unit of the communications system of FIG. 1.

FIG. 3 illustrates two symbol constellations that are transmitted in two separate frequency bins in accordance with OFDM/DMT data modulation techniques.

FIGs. 4 and 5 illustrate exemplary bandwidth allocations for the local cable system and the cable telephony system, respectively.

FIGs. 6 - 8 illustrate various embodiments of the receiver of the remote service unit at various levels of detail.

FIGs. 9 - 11 illustrate various embodiments of the transmitter of the remote service unit at various levels of detail.

FIGs. 12 - 15 illustrate various aspects of one embodiment of a partial sequence filter that may be used in either the head end unit or the remote service unit.

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FIGs. 16 - 22 illustrate a system that may be used to, inter alia, attain upstream and downstream symbol alignment between the head end unit and a newly added remote service unit to thereby initialize communications.

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## DETAILED DESCRIPTION OF THE INVENTION

FIG. 1 is a block diagram of a multi-point communications system which may use a remote service unit having the improved receiver and transmitter architectures disclosed herein. As illustrated, the communications system, shown generally at 20 includes a head end unit (HE) 25 disposed at a primary site. The head end unit communicates with a plurality of remote service units (RSUs) 30 respectively disposed at a plurality of secondary sites, over a transmission medium 35 such as a coaxial cable.

The digital communications system 20 may, for example, be a cable telephony system. In such an application, the head end unit 25 is disposed at a cable television transmission facility while the remote service units 30 are disposed at individual customer locations, such as individual customer homes. The transmission medium 35 would be the new or existing transmission cable used to transmit the cable television services. The head end unit 25 in a cable telephony network is responsible for communicating with and interconnecting telephone calls between the plurality of remote service units 30 as well communicating with a central switching office 40 for sending and receiving telephone calls from sites exterior to the local cable television service area.

A block diagram of one embodiment of a head end unit 25 and a remote service unit 30 is shown in FIG. 2. As illustrated, the head end unit 25 and the remote service units 30 each generally comprise respective baseband sections 45, 50 and respective RF sections 55, 60. The baseband section 45 of the head end unit 25 receives constellation data at one or more lines 65 and



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performs an Inverse Fast Fourier Transform on the received data. The transformed signal is modulated within the RF section 55 for transmission along the cable transmission 35. The remote service units 30 receive the RF modulated data from the cable transmission medium 35 in the respective RF section. The received signal is demodulated within the RF section 60 of the remote service unit 30 and the resulting signal is supplied to the baseband section 50 which performs a Fourier Transform on the signal to recover the data transmitted by the head end unit 25. The recovered data is supplied from the baseband section 50 along one or more lines 70 for further decoding. As is apparent from the block diagram of FIG. 2, constellation data may also be received at one or more lines 75 of the baseband section 50 of the remote receiving unit 30. The received data undergoes an Inverse Fourier Transformation or, more preferably, a direct sequence transformation and the resulting signal is RF modulated for transmission along the cable transmission medium 35 for receipt by the head end unit 25. The head end unit 25 demodulates the received signal in the RF section 55 and performs a Fast Fourier Transform on the demodulated signal to recover the transmitted data and provide it on one or more lines 80 for further decoding.

The present system 20 utilizes OFDM/DMT digital data modulation for exchanging communications data between the head end unit 25 and the remote service units 30. Such OFDM/DMT digital data communications assign a particular amplitude, frequency, and phase for each transmitted “sub-symbol”. The transmitted “sub-symbol” represents one or more information data bits that

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are to be transmitted between the units 25 and 30. Each sub-symbol may be represented by a point within a "constellation", the point being transmitted at a given carrier frequency or "bin". FIG. 3 illustrates the use of two constellations 90 and 95, each having sixteen constellation points that are capable of being transmitted within two separate frequency bins. As illustrated, a sub-symbol having a carrier signal of frequency  $f_1$  has its amplitude and phase varied depending on the constellation point that is to be transmitted. For example, a constellation point representing the binary states 0000 is transmitted as a sub-symbol at a phase of  $\theta_1$  and an amplitude of  $A_1$  during a designated symbol time. A constellation point representing the binary states 1111, however, is transmitted as a sub-symbol at a phase of  $\theta_2$  and an amplitude of  $A_2$  during a designated symbol time. Similarly, the second constellation 95, preferably having the same amplitude and phase designations for its sub-symbols as the first constellation 90, is used to modulate a second carrier frequency  $f_2$ . The resulting modulated signals are combined into a single output symbol in which the individual sub-symbols are differentiated from one another based on their respective carrier frequencies or "bins". It will be recognized that many variations of the disclosed OFDM/DMT transmission scheme are possible, the foregoing scheme being merely illustrated herein to provide a basic understanding of OFDM/DMT communications.

Referring to FIG. 4 there is shown an exemplary break-up of the bandwidth allocated to a local cable television service. As illustrated, the entire allocated bandwidth is further sub-allocated into smaller bandwidth portions for

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the transmission of selected services such as cable television, audio broadcasting, cable telephony, and other miscellaneous services. The bandwidth allocated for cable telephony constitutes the focus of further discussion. However, it will be recognized that the digital communications system described herein can be utilized in any multi-point digital data communications system.

FIG. 5 illustrates the bandwidth allocated, for example, to the cable telephony communications. Without limitation, the bandwidth of the exemplary embodiment may be about 2 MHz with a center frequency of about 600 MHz. As shown, the bandwidth is divided into a plurality of frequency bins 100, each bin carrying a sequence of sub-symbols corresponding to the data that is to be communicated. The head end unit 35 sends and receives data to and from multiple remote service units 30 and must be capable of processing substantially all, if not all of the bins allocated to cable telephony transmission. Accordingly, the head end unit 25 must have a substantial amount of processing power. Such a high amount of processing power naturally gives rise to increased production, maintenance, and power costs. Similarly, the remote service units 30 require substantial processing power if they are to each process the entire bandwidth or number of bins allocated to the cable telephony communications and transmitted by the head end unit 25.

The present inventors, however, have recognized that many applications using multi-point, OFDM/DMT data communications do not require that the remote service units 30 process the entire number of bins transmitted by the

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transmitter at the primary site. Rather, as recognized by the present inventors, the remote service units 30 employed in many types of OFDM/DMT data communications systems, such as cable telephony systems, need only be capable of processing a limited number of bins of the entire number of bins transmitted by the head end unit 25.

Based on this recognition, the remote service units 30 are designed to process substantially fewer bins than the entire number of bins transmitted by the head end unit 25. More particularly, the receiver architecture of each RSU is particularly adapted to exclusively digitally process only a limited number of bins of the larger number of OFDM/DMT bins that are transmitted by the head end unit 25. Remote service units 30 disposed at different secondary sites are preferably designed to process different subsets of bins. More preferably, the particular subsets of bins processed by any remote service units is dependent on command transmissions received from the head end unit 25.

Such a receiver architecture has several advantages. For example, the digital signal processing capability required by the receiver of each RSU is significantly reduced thereby making each RSU more economical to design, manufacture, and maintain. Additionally, each RSU consumes less power than would otherwise be required if each RSU had to process the complete number of bins sent by the head end unit 25.

FIG. 6 is a schematic block diagram of one embodiment of a receiver 110 suitable for use in the remote service units 30. As illustrated, the exemplary embodiment is comprised of five functional sections: an RF

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conversion section 115, an IF-to-digital conversion section 120, a Fourier Transform section 125, a decoding and framing section 130, and a timing and control logic section 140.

The RF conversion section 115 receives the RF signal from the transmission medium 35 through, for example, a splitter, and transposes the desired part of the OFDM/DMT spectrum containing the information that is to be recovered into a predetermined intermediate frequency (IF) pass band. As will be readily recognized, and as will be set forth in further detail below, the RF conversion is achieved with a combination of mixers, filters, and frequency synthesizers.

The IF-to-digital section 120 is used to sample the IF analog signal output of the RF conversion section 115 and provide a digital output signal corresponding to fewer than all of the bins transmitted by the head end unit 25.

The resulting digital output signal can thus be processed by the Fourier Transform section 125 using substantially less processing power than would otherwise be required to process the full number of bins. The desired output signal is achieved by band pass filtering the signal to provide a signal that comprises a subset of the original OFDM/DMT bins transmitted by the head end unit 25. This filtered signal is then under-sampled such that the desired signal folds down to near base band via an aliasing process. Under-sampling permits the use of a lower frequency A-to-D conversion than would otherwise be required. Additionally, the under sampling reduces the number of digital samples that are generated, thereby reducing the amount of processing power

required in subsequent digital processing steps in the Fourier Transform section 125.

It will be recognized, however, that under sampling is not the only choice for reducing the number of digital samples that are generated to the subsequent sections. For example, a mixer could be used to mix the filtered signal to base band thereby reducing the sampling frequency required to properly sample the received signal. This too would allow one to take advantage of the reduced bin receiver to reduce speed, complexity, and power usage of the system.

The Fourier Transform section 125 is used to take the Fourier transform of the sampled signal output from the IF-to-digital section 120 in order to obtain a frequency domain representation of the OFDM/DMT modulated signal. This can be achieved in any one of multiple ways. First, the Fourier Transform section 125 may include a digital signal processor that performs a Fourier Transform on the sampled data. However, unlike ordinary OFDM/DMT digital communications which perform a Fast Fourier Transform over all the bins sent by the transmitter at the primary site, the Fourier Transform implemented by the presently disclosed receiver 110 is taken over a reduced number of bins. This results in significant cost and power savings. A further improvement can be achieved in the case where the sampled signal received from the IF-to-digital section 120 contains more bins than any individual receiver needs to receive. In this case, a hardware correlator could be used to obtain a Fourier Transform of only the bin frequencies containing data that the

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receiver 110 is to recover. This permits further power and complexity reduction when the narrow band receive window is still somewhat larger than the needed bandwidth. Furthermore, this architecture allows the speed and power consumption to be scaled according to the number of bins any particular receiver needs to receive.

It will be recognized that an FFT can be performed on the reduce subset of received bins yet still reap the advantages inherent in the disclosed receiver architecture. This is due to the fact that the FFT can be implemented using a digital signal processor of reduced complexity when compared to an FFT processing the entire bandwidth transmitted by the head end unit 25.

The decoding and formatting section 130 receives the processed output of the Fourier Transform section 125 and converts the received frequency domain constellation points into the corresponding data they represent thereby completing the recovery of the transmitted data. The decoding and formatting section 130 also performs any error correction, digital equalization, slicing to bits, framing, and descrambling that is required. Such decoding and formatting, as is readily recognized, is dependent on the framing and formatting used by the head end unit 25 in transmitting the data and may take on any form.

It is worth noting that phase compensation can be implemented in the decoding and formatting section 130 to compensate for any differences between the mixing frequencies of the transmitter of the head end unit 25 and the mixing frequencies of the receiver of the remote service unit 30. Such phase compensation can be implemented by effectively rotating the phase of each

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received sub-symbol through a predetermined phase angle  $\theta_3$  during each symbol period. As such, the phase angle through which each sub-symbol is rotated is a multiple of  $\theta_3$ . For example, a first sub-symbol during a first symbol period T1 is rotated by phase angle  $\theta_3$ , while the sub-symbol received during a subsequent second symbol period T2 is rotated by a phase angle equal to  $2 * \theta_3$ .

The output from the decoding and formatting section 130 is supplied to the input of one or both of an analog-to-digital section 132 and direct digital section 137. The analog-to-digital section 132 converts the digital information received from the decoding and formatting section 130 to an analog signal that may be supplied to various analog devices. The direct digital section 137 provides an interface between the digital signal output of the decoding and formatting section 130 and any digital data devices.

A centralized timing and control block 140 is used in the illustrated embodiment to provide the timing and control signals required to coordinate the operation of the other processing sections. It will be recognized, however, that this timing and control function may also be performed in a decentralized way, wherein each of the individual processing sections 115, 120, 125, and 130 contain or share individual timing and control circuitry. However, in such instances, additional synchronization circuitry dealing with the resulting asynchronous nature of the clocks in the individual sections may be required. Such a decentralized architecture could also require more pipelining with its



associated memory.

FIG. 7 illustrates one manner in which the RF section 115, the IF-to-digital section 120, and a portion of the Fourier Transform section 125 can be implemented. As shown, the signal transmitted from the head end unit 25 is received by a first bandpass filter 150 that, for example, has a wide pass band with end frequencies of about 470 MHz and 750 MHz. The signal from the bandpass filter 150 is supplied to the input of a tuner 155 that has its characteristics determined by the output of a tuner synthesizer 160 that is tied to receive the output of a reference clock that, for example, has a clock frequency of about 4 MHz. Without limitation, the tuner 155 mixes the signal from the bandpass filter 150 to a signal having a frequency of about 240 MHz. The output of the tuner 155 is supplied to the input of a further filter 165, a SAW filter in the illustrated embodiment. The output of SAW filter 165 is supplied to an IF mixer 170 that transposes the signal to an intermediate frequency (IF) of, for example, 10.7 MHz. The mixer 170 performs the IF conversion by mixing the signal received from the SAW filter 165 with the signal generated by oscillator 175. The signal generated by the oscillator 175 is synchronized to the reference clock signal received on line 180.

The received signal, now converted to the IF band, is subsequently supplied to the input of an IF bandpass filter 185 that, for example, has a 300 KHz bandwidth and a center frequency of about 10.7 MHz. The output of the bandpass filter 185 is an OFDM/DMT modulated signal having only a subset of the entire number of bins transmitted by the head end unit 25. One or both of

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the filters 165 and 185, however, may be used to reduce the bandwidth of the received signal so as to limit the number of bins that are ultimately processed. The filtered IF signal is converted to a digital signal by an A / D converter 190 that has its conversion clock on line 195 synchronized to the reference clock on line 180 through a clock dividing circuit 200. As noted above, the conversion clock frequency may be selected to be low enough to result in undersampling of the IF signal thereby reducing the number of samples supplied at the A/D converter 190 output. An increased in the sampling rate, however, can be used to compensate for any inexactness of filters 165 and/or 185.

The output of the A/D converter 190 is supplied to the input of a digital signal processing circuit 205 that generates the Fourier Transform of the signal that it receives, extracts the received symbols based on the Fourier Transform information, and performs any other processing functions required. In a cable telephony system, the output of the digital processing circuit 205 may be supplied to the inputs of one or more D/A converters or CODECs that convert the data contained in the received symbols to one or more analog output signals, such as audio voice signals, that can be heard by a person engaged in a telephone conversation.

FIG. 8 illustrates one embodiment of a hardware correlator 210 that may be used in the Fourier Transform section 125. The illustrated hardware correlator 210 is designed to correlate nine frequency bins within the total bandwidth of frequency bins that are provided in digital format at the output of the A/D converter 190 of, for example, the IF-to-digital circuit 120. The

correlator 210 includes a multiplier section 215, a frequency generator section 220, and an accumulator section 225. As shown, the multiplier section 215 receives the digital data that is output from the IF-to-digital section 125 and multiplies each value by the sine and cosine value of each of the nine frequency bins. The sine and cosine values are supplied as inputs to the multiplier 215 from the frequency generator section 220. The frequency generator section 220 includes a step-size register 227 that includes, in the present embodiment, nine register locations that are programmed by a microcontroller or digital signal processor. The values stored in the step-size register 225 are used to determine the step-size of the addresses supplied to address the data in a cosine table ROM 230, shown here has a quarter wave cosine table. An address modifier circuit 235 receives the address data from the address register 240 and modifies the data so that the address data supplied to the cosine table ROM 230 falls within an acceptable range of addresses and thereby accesses the proper portion of the wave. A sine/cosine bit is supplied from, for example, the timing and control circuit 140 so that each value received from the IF-to-digital converter 125 is multiplied by both the sine and cosine values of each of the nine frequency bins. The data resulting from the multiplication operation are accumulated in the accumulator section 225 and output to the decoder/formatting section 130 for further processing.

One embodiment of a transmitter suitable for use in the remote service units 30 is illustrated in FIG. 9. The transmitter, shown generally at 300 transmits its digital data in an OFDM/DMT modulated format using a number

of bins that is less than the number of bins transmitted and received by the head end unit 25. Accordingly, the transmitter 300 can generate the OFDM/DMT transmission output by modulated direct digital synthesis.

The transmitter 300 of the illustrated embodiment is designed to accept both analog and digital signal information for OFDM/DMT transmission. Accordingly, the transmitter 300 includes an analog-to-digital interface unit 305 and a direct digital interface unit 310. The analog-to-digital interface unit 305 is used to sample an analog signal, such as a voice signal of a person engaged in a telephone conversation, and convert it to digital data to be transmitted. For example, the analog-to-digital interface unit 305 may contain CODECs and SLICs for connecting one or more telephones to the system.

The direct digital interface unit 310 interfaces with any type of device that provides a signal that is already in digital format. For example, the direct digital interface unit 310 might have a serial interface for receiving data, as in a modem application. The unit 310 might also receive data from a system CPU to be sent to the receiver of the head end unit 25.

The transmitter 300 also includes a data interface unit 315. The data interface unit 315 receives data from any combination of the following: sampled analog data from the output of the analog-digital interface unit 305, direct digital data from the output of the direct digital interface unit 310, or other digital data sources that, for example, provide system communication information generated from within or without the data interface unit 315. The data interface unit 315 formats the data received from these data sources into a

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single data stream. Tasks such as data framing, scrambling, error correction coding, CRC generation, data synchronization, and stuffing may be performed by the data interface unit 315 as part of the formatting function. Optionally, the data interface unit 315 may group the data into words that represent the unique constellation points to be transmitted. As will be readily recognized, the specific formatting operations executed by the data interface unit 315 are dependent on the particular requirements of the communications system in which the remote service unit 30 is employed.

The serial data stream output from the data interface unit 315 is supplied to the input of the transmit engine circuit 320. The data that the transmit engine circuit 320 receives includes one constellation point for each OFDM/DMT bin of the reduced set of bins that is active during a single symbol time. The transmit engine circuit 320 is responsible for calculating the Inverse Fourier Transform on the data stream that is to be modulated and for producing a time domain sequence for each symbol along with any cyclic prefix.

Generally, systems using OFDM/DMT modulation performs this function using an IFFT that is implemented, for example, with a digital signal processor.

However in a multi-point application, such as the communication system disclosed herein, only a limited number of the possible frequencies or bins are used by each secondary transmitter. Given that only a portion of the total available transmission bandwidth is utilized, the disclosed secondary transmitter architecture is more efficient and cost-effective.

In the preferred embodiment of the transmit engine circuit 320, the time

domain sequence is generated by modulated direct digital synthesis, sample by sample. In addition to reducing the complexity of the transmitter, this operation reduces system latency. The time domain sequence for a given symbol is created by generating sine waves, sample by sample, and adding them together. The frequency determines the bin in which the data will be received. The phase and amplitude are used to convey the data intelligence.

Additionally, the preferred embodiment of the system is such that there are 256 bins between 0 Hz and the Nyquist frequency. This is typical in OFDM/DMT systems. That is, the spectrum between 0 Hz and the Nyquist frequency is divided into a number of bins wherein the number is a power of 2, i.e.  $2^n$  where  $n$  is an integer. This facilitates the use of FFTs and IFFTs. However, the presently disclosed transmitter 300 preferably uses a Nyquist frequency that is greater than the transmit bandwidth, thereby leaving a number of bins turned off on each edge. Such a transmission scheme provides a natural filtering effect at the edges of the bandwidth. In the preferred embodiment, 209 bins fit within the allocated transmit bandwidth. An additional eight bins are turned off on either end of that bandwidth to leave some transition bandwidth for filters.

Optionally, the transmitter 300 may utilize a digital filter 325 that receives the output of the transmit engine circuit 320. This optional filter performs any desired digital filtering of the output stream and, for example, may be useful in further limiting the bandwidth of the signal. The filter 325 may be, for example, a digital partial sequence filter with reduced complexity.

Such a digital partial sequence filter is set forth below.

The digital sequence output from either the digital filter 325 or the transmit engine circuit 320 is supplied to the input of a digital-to-baseband converter or a digital-to-IF converter 330 depending on whether the signal output is at an IF or at baseband. The converter 330 includes components that perform digital-to-analog conversion and analog filtering. If the output is at an IF, a bandpass filter centered around any image of the output spectrum may be employed. This results in an IF signal that is more easily processed in subsequent operations.

The output of the converter 330 is supplied to the input of an RF frequency converter 335. The RF frequency converter 335 shifts the OFDM/DMT spectrum from IF or baseband to the desired RF frequency. As will be readily recognized, the RF frequency converter 335 may be implemented using a combination of mixers, filters, and frequency synthesizers to implement the conversion functions and provides an OFDM/DMT output that is suitable for transmission along the transmission medium.

Timing and control of the transmitter system 300 is provided by a common timing and control logic circuit 340. A centralized timing and control circuit 340 is used in the illustrated embodiment. This function, however, could also be performed in a decentralized way. If decentralized timing and control are utilized, the timing and control circuits would likely be more complex to deal with the resulting lack of synchronism between circuits. It could also require more pipelining with its associated memory.

One embodiment of digital transmission circuitry that may be used to generate the digital OFDM/DMT signal for subsequent D/A conversion and RF modulation is set forth in FIG. 10. The digital transmission circuitry 350 illustrated here may be used to implement, inter alia, the transmit engine circuit 320 of FIG. 9. The digital transmission circuitry 350 accepts digital data from, for example, the output of first and second CODECs respectively associated with individual first and second telephones. Additionally, the circuitry 350 may receive digital data that is to be transmitted in embedded control channels within the transmitted signal, each of the embedded control channels being respectively associated with one of the first and second telephones. The digital data output from the CODECs and on the embedded control channels are combined together by a combiner circuit 360 into two separate data groups, illustrated here as DATA1 and DATA2. The presently disclosed embodiment provides the capability of generating OFDM/DMT transmissions in one or more of nine frequency bins.

Each data group DATA1 and DATA2 is supplied to the input of an encoder logic circuit 365. The encoder logic circuit 365 divides the data groups into symbol groups and maps each symbol to a point of a constellation to obtain a phase and amplitude for each symbol. The amplitude information for each symbol is provided on one or more lines 370, while the phase information for each symbol is provided on one or more lines 375.

Generation of the desired frequency and phase for each symbol takes place through the interrelated operation of the start address selection ROM



380, the step size selection register 385, adder 390, address register 395, address modifier 400, and sine table ROM 405. The sine table ROM 405 contains the digital data representation of a sine wave, or selected portion thereof, shown here as a quarter wave table, in successive addressable memory locations. The successive, addressable memory locations of the sine table ROM 405 are addressed in a specific manner to provide a digital output signal having the phase and frequency characteristics of the symbol that it is to represent. The phase of the sine wave represented by the digital output signal is dependent on the memory location that is first addressed at the beginning of the symbol period while the frequency of the sine wave is determined by the step size used to address successive memory locations within the sine table ROM.

The selection of the memory location that is first addressed at the beginning of a symbol period is dependent on the phase information on output lines 375 of the encoder logic circuit 365. The phase information is supplied to the start address ROM 380 which provides a start address which is output to the address storage register 395. The step size through which the memory locations within the sine table ROM 405 are to be cycled is determined by the value at the output of the step size storage register 385. The step size storage register 385 includes one or more memory storage locations that are accessible to a microcontroller or DSP. The microcontroller determines the step sizes that are stored in the step size storage register 385 based on the desired symbol carrier frequency bins that can be used - the larger the step size, the higher the carrier frequency. In the illustrated embodiment, the step size register 385

includes nine register locations for the nine bins that can be transmitted. Preferably, the step size register 385 is programmed by the microcontroller based on commands received from the head end unit 25. The step size value is supplied at one or more output lines 410 of the step size register 385 to the input of the adder 390. The adder 390 functions to provide the address signals that are used to successively address the memory locations of the sine table ROM 405. Accordingly, the output of the address register 395 is fed back to the input of the adder 390 so that the sine table ROM 405 selection address is incremented by the appropriate step size on each successive addressing cycle corresponding to the particular frequency bins.

Since the sine table ROM 405 of the present embodiment only contains a portion of a single sine wave, an address modifier 400 is used. The address modifier 400 includes combinatorial and/or programmed logic circuits that perform calculations that ensure that the address value supplied to the sine table ROM 405 falls within an acceptable range and thereby accesses the appropriate portion of the wave. Such calculations ensure that the newly calculated address starts at the appropriate portion of the sine table ROM 405 without generating an undesired discontinuity.

The output of the sine table ROM 405 is supplied to the input of a multiplier 420. The multiplier 420 accepts each digital data value that is output from the sine table ROM 405 and multiplies each value by the corresponding amplitude factor as determined from the amplitude information output of the encoder logic circuit 365 received along lines 370.

Since the sine table ROM 405 of the presently disclosed embodiment includes only positive values, some circuitry must be provided to generate the negative portions of the wave. To this end, the output of the multiplier 420 is supplied to a two's complement converter 430 and the most significant bit (MSB) from the address register 395 is used to signal the converter 430 to either through-connect the output of the multiplier 420 to an accumulator 440 or perform a two's complement operation on the output before providing it to the accumulator 440. The accumulator 440 adds all of the data points for the nine frequency bins that are generated during a single sample period and provides the resulting data on output lines 445.

As will be readily recognized, the timing and control inputs from the timing and control logic circuitry 340 are not illustrated in FIG. 10. Such inputs have been omitted in order to simplify the figure. Given the foregoing description, the timing and control operations can be readily derived.

FIG. 11 shows yet a further embodiment of the basic elements of the transmit engine shown in FIG. 10. In the embodiment of FIG. 11, a full wave sine table ROM 500 is utilized. Accordingly, the two's complement circuit 430 and the address modifier 400 are not provided.

With reference to FIG. 9, the digital filter 325 may be a partial sequence filter as shown generally at 600 of FIG. 13. The basic operation of a partial sequence filter 600 can best be understood in connection with the waveforms illustrated in FIG. 12. Line 605 of FIG. 12 is a time domain signal representing one bin of an OFDM/DMT signal over three symbol periods. As shown, the

FIG. 10

beginning of each symbol signal is generally discontinuous to the preceding symbol signal and the end of each symbol signal is generally discontinuous to the beginning of the subsequent symbol signal. The discontinuities between symbols result in a generally broad-band frequency spectrum which the digital filter 325 is designed to limit.

The digital filter 325 may be implemented as a finite impulse response (FIR) filter. Typically, a FIR filter is expected to process all of the digital samples provided by the transmit engine of the preceding stage. That is, all of the digital samples that are output from the transmit engine 320 are supplied to the input of and are processed by the FIR filter. Such a FIR filter thus requires a substantial amount of processing power. For example, a 101 tap FIR filter responsive to a digital signal having a 10 MHz sampling frequency would typically require approximately 1000 MIPS to perform the requisite multiplication. If the filter is symmetric, the complexity can be reduced so that 500 MIPS are required to perform this multiplication. In either instance, such a filter implementation may be quite costly, particularly in a multi-point digital communications system.

The present inventors have recognized a unique characteristic of DMT/OFDM signals and have used this characteristic to reduce the complexity of the filter. With reference to FIG. 12, the present inventors have recognized that the OFDM/DMT signal looks like a tone during a substantial portion of the middle of the symbol period. The discontinuities that broaden the frequency spectrum of the transmitted symbols occur only at the beginning portion and

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end portion of the symbol period. In view of this characteristic, the inventors have recognized that, when the taps of a FIR filter are inside of a single symbol, the filter's output is approximately the same as the input. This relationship exists when the FIR filter has unity gain and exhibits linear phase in the pass band. As such, a FIR filter does not alter signals within the pass band and need only perform filtering of samples taken at the beginning portion and end portion of a symbol period.

In view of the foregoing characteristics, the inventors have recognized that the filter 325 may be a partial sequence filter that digitally filters only a select portion of the samples of a symbol period. In an OFDM/DMT system, such as the one disclosed herein, the partial sequence filter digitally filters only the samples occurring at a beginning portion of the sample period and an end portion of the sample period. For example, if a 101 tap FIR filter is used in the disclosed system, it becomes possible to only digitally process 100 of the 1100 samples in every symbol period, 50 samples at the beginning portion of a symbol period and 50 samples at the end portion of a symbol period. Such an approach reduces the number of multiplies that must be executed by a factor of 100/1100, resulting in only approximately 9% of the complexity that would otherwise be required if all 1100 samples were processed. The result is a reduction from 1000 MIPS to 91 MIPS. The complexity may be further reduced using standard filtering techniques that can be used for FIR filters with symmetric taps. Since sample 1 is multiplied by the same coefficient as used with sample 101, sample 1 may be added to sample 101 before multiplication.

Likewise, sample 2 is multiplied by the same coefficient as sample 100 and, as such, sample 2 may be added to sample 100 before multiplication. This symmetrical relationship can be used for approximately all of the processed samples. Application of this principle further reduces the complexity to 45 MIPS.

The partial sequence filtering can be implemented by dedicated hardware or with a digital signal processor. For example, a digital signal processor within the head end unit 25 may be used to implement the partial sequence filter. Alternatively, a dedicated hardware circuit, such as the one illustrated in FIG. 13, may be used to implement the partial sequence filter.

FIG. 13 illustrates an exemplary implementation of the partial sequence filter. As illustrated, the partial sequence filter, shown generally at 600, receives blocks of data from a preceding IFT process, such as the process performed by the transmit engine 320. As noted above, the IFT takes the inverse Fourier transform for a set of constellation points that make up a given symbol. A new block of samples is generated once for every symbol. After each symbol undergoes an IFT, the time domain data is written to either symbol buffer 610 or symbol buffer 615, alternately. It may be advantageous to use a cyclic prefix at the start of every symbol. Such a cyclic prefix is described below. In such instances, the end of the sequence generated by the preceding IFT process is tacked onto the beginning of the time sequence and functions as the cyclic prefix.

The partial sequence filter 600 is comprised of symbol buffers 610 and

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615, a filter engine, shown generally at 620, a multiplexer 625, and an output register 630. Generally stated, after undergoing a preceding IFT process, the digital data for each symbol is alternately stored in either symbol buffer 610 or symbol buffer 615. The IFT processed symbol data for each symbol is supplied from one or the other of the symbol buffers 610, 615 to either the input of the filter engine 620 for filter processing and subsequent supply, for example, to the digital-to-baseband (or IF) circuit 330, through output register 630 or directly, without filtering, for supply to circuit 330 through output register 630. Only selected portions of the data within a given symbol buffer are supplied for filtering to the input of the filter engine 620, the remaining data being bypassed around the filter engine 620 for supply to the input of circuit 330. The bypass operation is facilitated by selection of the appropriate data through multiplexer 625.

As illustrated, the transmit engine 620 is comprised of registers 635 and 640, adder 645, digital multiplier 650, coefficient data table memory 655, adder 660, feedback register 665, and engine output buffer 670. Together, the adder 660 and feedback register 665 constitute an accumulator 675. With respect to the particular embodiment of the filter engine illustrated here, it is assumed that the filter is symmetric so that the coefficient for FIR filter tap 101 is the same as the coefficient for FIR filter tap 1. Likewise, the coefficient for tap 100 is the same as that of tap 2.

In operation, given the foregoing assumptions, the sample needed for tap 101 is first latched into register 635. The sample needed for tap 1 is then

latched into register 640. The two samples are added to one another by adder 645. The resulting sum is supplied to the input of digital multiplier 650 where it is multiplied by the coefficient for tap 1 as supplied from the coefficient table memory 655. The resulting digital value is effectively stored in register 665 of the accumulator 675 (the initial value contained in register 665 is assumed to be zero). The same basic operation is next performed for the samples needed for taps 2 and 100, but using the coefficient for tap 2 as supplied from the coefficient table memory 655. The digital value resulting from the multiplication with the coefficient for tap 2, however, is added to the digital value result of the previous multiplication that is already stored in register 665 by the accumulator 675. In the exemplary embodiment, this operation is repeated for a total of 50 times. The 51<sup>st</sup> operation proceeds in a slightly different matter. More particularly, the data corresponding to tap 51 is stored in register 635, while register 640 is loaded with a zero. These values are added to one another by adder 645 and are multiplied by tap coefficient 51 at multiplier 650. The resulting value is added to the digital value that is already present in register 665. The result is again latched into register 665. As such, register 665 contains a filtered output value. This filtered output value is subsequently stored in the engine output buffer 670 for subsequent supply to the D/A converter of the digital-to-baseband (or IF) circuit 330 through multiplexer 62 history5 and register 630.

FIGs. 14 A-E illustrate data passing through the filter engine 620 of the illustrated partial sequence filter 600 having a 101 tap FIR filter. To obtain an



output sample from the filter, each tap multiplies the corresponding data and the results of these multiplication operations are summed together. In FIGs. 14 A-E, the data samples are denoted as X:Y, where X represents the symbol number and Y represents the sample number for the particular symbol. For example, the notation 1:1000 represents the 1000<sup>th</sup> sample of symbol number one. Each tap is denoted by a numbered box, and the particular data sample present at a given tap is shown therein to indicate the positions of the data samples within the filter at a given time. For example, at the time designated by the filter state represented in FIG. 14A, tap 1 is multiplying sample 2:0, tap 2 is multiplying sample 1:1099, etc..

With reference to FIG. 14A, the filter contains data from both symbol number 1 and symbol number 2. As shown, the first sample of the second symbol, 2:0, has just entered the filter engine and is multiplied by the coefficient for tap 1. All of the other taps multiply samples from the previous symbol, symbol number 1. The digital filter output, which is the sum of all of the multiplications, replaces sample 1:1050 for D/A conversion. In the specific example illustrated here, the output of the filter will always replace the data sample that is in the box corresponding to tap 51.

FIGs. 14 B-E illustrate subsequent operations of the filter. More particularly, FIG. 14B illustrates the state of the filter in an operation immediately subsequent to the filter state shown in FIG. 14A. FIG. 14C illustrates the state of the filter for the last sample from symbol 1 (1:1099) that needs to be replaced. FIG. 14D shows the state of the filter for the first sample

from symbol 2 (2:0) that needs to be replaced on the way to the D/A converter of the circuit 330. Finally, FIG. 14E shows the state of the filter for the last sample that needs to be replaced in the first fifty samples of symbol number 2 (2:49). The last 50 samples of symbol number 2 also require filtering and would be processed accordingly.

To function properly, the partial sequence filter should be designed to have an amplitude and phase effect in the pass band. Absent such effects, a significant discontinuity will exist between the filtered and unfiltered data. Such discontinuities may result in both in-band and out-of-band noise.

Coordination of the overall timing and control, including the reading and writing of the symbol buffers 610 and 615, control of the state of the filter engine 620, control of the multiplication and summing operations, and selection of filtered or unfiltered data for output to the D/A converter of circuit 330 are performed by the timing, address generation, and control logic circuit 690 (control logic unit). The control logic unit 690 coordinates the reading and writing of the symbol buffers 610 and 615 with receipt of data samples from the preceding IFT process to ensure that the IFT process is complete and that the samples are at least beginning to be written to one of the symbol buffers before those samples are needed at the output register 630. The control logic unit 690 should also ensure that the samples in one or the other of symbol buffers 610, 615 are supplied to either the filter engine 620 or the output register 630 before they are overwritten by the symbol data from the subsequent IFT operation. Additionally, the control logic unit 690 should coordinate movement of the data

through the partial sequence filter so that data is available to the filter engine 620 at a rate which allows the filter engine to run at a moderate rate over the majority of the symbol period.

The control logic unit 690 should control the relationship between the read and write pointers associated with each of the symbol buffers 610 and 615 and the engine output buffer 670 so as to minimize latency. However, latency can be added to the system design to reduce timing constraints.

FIG. 15 illustrates the relationship between some of the buffer read and write pointers. In the illustration, the timing between the pointers is shown near the buffer boundaries. In a preferred embodiment of the partial sequence filter, the read pointer 705 that gets the data from the engine output buffer 670 for supply to the output register 630 is also used to read data from each of symbol buffers 610 and 615. The read pointer 705 gets data samples X:50 - X:1049 from one or the other of symbol buffers 610 and 615 (depending on where symbol number X is stored), and gets data samples X:0 - X:49 and X:1050 - X:1099 from the engine output buffer 670. The appropriate samples should always be available to the output register 630 for subsequent processing. To reduce latency, however, the samples are processed as close to just-in-time as practical.

The exemplary pointer locations illustrated in FIG. 15 show the pointers near crossover points to illustrate how close the pointers can come to one another. In the exemplary illustration, the filter engine 620 has just completed the writing of the outputs that will replace sample 4:49 and has begun

processing the 4:1050 replacements. The read pointer 705 is just beginning to read sample 4:49 from the engine output buffer 670. Meanwhile, the write pointer 710 has just finished writing sample 5:49 so that the filter engine has every sample required to process the 4:1050 replacement.

FIGs. 16 - 18 illustrate one manner of initiating communications between a newly added or powered-up remote service unit 30 and the head end unit 25. As shown at step 720, the remote service unit 30 first synchronizes its internal clocks with the head end unit 25. One way in which this may be accomplished can be described with reference to FIG. 2 which shows a pilot tone added by the head end unit 25 to a predetermined bin output that is transmitted to the remote service units 30. The pilot tone is extracted from the received signal by the receiver of the remote service unit 30 and used, for example, as a reference signal for a phase-locked-loop circuit 600. The output of the phase-locked-loop 600 is provided to the input of a voltage controlled oscillator 605 which generates the reference clock for the remote service unit 30.

After the clock synchronization of step 720 is completed, the remote service unit 30 acquires its symbol timing at step 730. One way in which symbol timing may be acquired is by adding a predetermined coherent signal to selected symbol transmission frames. One such embodiment is illustrated in FIG. 17 which shows an impulse signal 800 being added by the head end unit 25 to the cyclic prefix CP of each symbol transmission. This impulse amplitude may be varied in accordance with a predetermined pattern. Preferably, the

impulse signal 800 reverses polarity with each successive symbol transmission so that a positive polarity impulse signal is added to the cyclic prefix of one symbol transmission while a negative polarity impulse signal is added to the cyclic prefix of the subsequent symbol transmission. Such an alternating polarity transmission assists in eliminating pilot tones, D.C. offsets, etc..

The receiver 110 of the remote service unit 30 finds the time location of the transmitted impulse signal by sampling, at a predetermined rate, the symbols that it receives and alternately adding and subtracting the samples of individual sample periods over several symbol periods. For example, the receiver 110 may sample the received signal at a rate of 100 samples per symbol period to generate samples  $SA_0 \dots SA_{99}$  during a first symbol period,  $SB_0 \dots SB_{99}$  samples that it receives during a subsequent symbol period,  $SC_0 \dots SC_{99}$  samples that it receives during a subsequent third symbol period, and so on. A first sum  $Y_0$  is generated from the first sample period of each sampled symbol period in accordance with  $Y_0 = SA_0 - SB_0 + SC_0 \dots$ . Each value of  $Y_N$  is determined based on a sum of  $L$  symbols, wherein  $L$  is the number of symbols required to produce a good estimate. Similar sums are generated for each of the sample periods through  $Y_{99}$  and the resulting sums are analyzed to determine where the peak amplitude occurs in the sampled symbol period. The time position of the peak amplitude corresponds to the time position of the added impulse signal and, thus, the time position of the cyclic prefix occurring at the beginning of each transmitted symbol. The receiver 110 can then make the requisite adjustments to ensure that it receives the symbols in proper

alignment.

It will be recognized that the foregoing manner of obtaining symbol alignment will function properly when there is no frequency shift between the bins that are transmitted by the head end unit 25 and the bins received by the remote service units 30. That is, any given bin occupies the same frequency location in the transmit spectrum at the head end unit 25 as well as at the receive spectrum at the remote service unit 30. However, there are certain situations in which a frequency shift in the received spectrum relative to the transmitted spectrum takes place. In one such situation, a frequency shift takes place when the receiver of the remote service unit 30 is to receive a selected window of transmitted bins but converts those bins to a normalized frequency range for subsequent processing.

To understand the foregoing, it is first recognized that the remote service unit 30 uses an RF mixer to down-convert the received passband signal to a pre-determined IF frequency which is then sampled and filtered to obtain the baseband signal (see FIG. 7). For a given RSU, the HE 25 transmits in a certain "window" of frequency bins. In the exemplary system discussed here, it will be assumed that there are eight windows (numbered 0-7), each spanning 26 frequency bins (250 KHz) (the exact number of bins and windows is not particularly relevant). The RSU 30 recognizes the number of the window that it is attempting to receive and is designed to process that window at a given baseband frequency. As such, no matter what window is used by the HE 25, the transmitted window of bins is received by the receiver at the same IF and,

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consequently, in a fixed part of the baseband spectrum. In order to do this, the mixing operation is carried out with an appropriate frequency offset. For example, if the beginning of each window is mapped to bin 64 within the receiver, the following window numbers, frequency bins, and offset bins would be utilized.

Window No.	Frequency Bins from the HE transmitter	Offset in Bins
0	18-44	46
1	44-70	20
2	70-96	-6
3	96-122	- 32
4	122-148	- 58
5	148-174	- 84
6	174-200	- 110
7	200-226	- 136

As such, a receiver that receives signals in Window No.1 would apply a positive 20 bin frequency shift to receive the signals beginning at bin 64 while a receiver that receives signals in Window No.7 would apply a negative 136 bin frequency shift to receive the signals beginning at bin 64. It will be readily recognized how such a frequency shift may be accomplished in the receiver architecture of Fig. 7.

Due to the presence of the cyclic prefix and the foregoing frequency offsets, the signals processed by the receivers of the remote service units experience a continuously accumulating phase offset for each symbol time. The phase offset is given by the equation:

$$\theta = 2\pi * (f_{\text{off}}) * (X_{\text{CP}}/N)$$

where  $\theta$  is in radians,  $f_{\text{off}}$  is the appropriate frequency offset in bins (e.g., from column 3 of Table 1),  $X_{\text{CP}}$  is the length of the cyclic prefix in samples and  $N$  is the length of a symbol in samples (without the cyclic prefix).

The foregoing phase offset effects the impulse response superimposed on the cyclic prefix as received by the receiver of a remote service unit 30. Accordingly, under such circumstances, the receiver must compensate for the phase offset if it is to properly detect the impulse signal and attain symbol alignment. To this end, the following steps are taken by the receiver and are illustrated in flow chart format in FIG. 16B.

1. Given a window number, the RSU determines the incremental (at symbol intervals) phase offset  $\theta$  corresponding to the particular window as described above.
2. After mixing with the appropriate frequency offset as described above, the receiver samples the baseband signal at a predetermined rate of, for example,  $K$  samples per symbol (including the cyclic prefix for each symbol).
3. The receiver creates two arrays  $XC$  and  $XS$ , each of  $K$  real numbers, in a sample by sample fashion. When the samples of the first symbol for



the symbol alignment are received, the arrays XC and XS are constructed by multiplying each of the K samples in a symbol by a pair of phase correction coefficients given by  $\cos(\theta)$  and  $\sin(\theta)$ , respectively.

4. For the next symbol, the phase correction coefficients are updated to be  $\cos(2*\theta)$  and  $\sin(2*\theta)$ , respectively. In general, for the lth symbol used in the process, the phase correction coefficients are given by  $\cos(l*\theta)$  and  $\sin(l*\theta)$ , respectively. Thus, for each symbol, the samples are multiplied by the corresponding updated phase correction coefficients as in step 3 above.

The receiver then denotes the kth sample of the two arrays using the lth symbol as  $CA_l[k]$  (e.g.,  $\cos(l*\theta)$ \* sample K of symbol l) and  $SA_l[k]$  (e.g.,  $\sin(l*\theta)$ \* sample K of symbol l), respectively, where the subscript l denotes the symbol for which these two arrays are created. Using a total of L symbols for averaging, form two arrays XC and XS according to

$$XC[k] = CA_1[k] - CA_2[k] + CA_3[k] - \dots + CA_L[k]$$

$$XS[k] = SA_1[k] - SA_2[k] + SA_3[k] - \dots + SA_L[k]$$

As above, L is the number of samples sufficient to provide a good estimate. These arrays are constructed in this manner due to the fact that the impulse signal alternates polarity on consecutive frames. Other array constructions may be used when other superimposed transmit symbol alignment patterns are used.

5. When the arrays XC and XS have been computed, compute an array Y by squaring and adding XC and XS sample by sample as follows:

$$Y[k] = XC[k]^2 + XS[k]^2.$$

6. Symbol alignment is then determined by the receiver using the array Y.

The preferred way to do this is to form a window of samples equal to the length of the cyclic prefix and slide it through the array Y. Each time that the window is moved, the receiver computes the total power (sum of squared values) in the window. The starting sample (i.e. the symbol alignment position) is taken to be the starting sample of the window having the largest power. In other words, the window with the largest power is aligned with the cyclic prefix samples frame transmitted by the head end unit. Another procedure that may be used to achieve the same goal is to first compute the peak amplitude position of the array Y. The sample position of the peak amplitude is then taken to be at a certain pre-determined location in the location of the symbol aligned cyclic prefix (usually near its center in a window receiver).

As noted above in step 2, K samples per symbol are used by the receiver. The preferred value is  $K = N_s/2$  where  $N_s$  is the number of samples per symbol. It is readily recognized, however, that if half the samples per symbol are used, the "resolution" of the process in finding the best symbol alignment degrades by a factor of two. If even lower values of K are used, there will be a proportional decrease in the resolution. To overcome this problem, the foregoing process may be slightly modified. For the preferred value of  $K =$

$N_s/2$ , the procedure may be modified by first processing as before with a pre-determined number of symbols until step 5. This results in the array  $Y$  of length  $K$  samples.  $Y$  is stored in memory and renamed for convenience as  $Y_{old}$ . Next, the samples used for steps 3-5 are offset by one from the sample locations used previously to compute  $Y_{old}$  and the process is repeated with the new sample locations in an identical manner as before and  $Y$  is recomputed.  $Y_{old}$  and  $Y$  are now interleaved (in accordance with the shift in one sample) to result in a new array of length  $2K$ . This double length array is now used in step 6 to determine the symbol alignment. Thus, at the cost of averaging over half the symbols for each of the  $Y$  arrays, the loss in resolution is overcome.

The phase coefficients used above may be generated in a number of manners. In accordance with a first method, the coefficients are generated "on the fly". To this end, a pair of memory locations in the receiver  $PC_0$  and  $PS_0$  are initialized with the values (1,0). Before the receiver is ready to process the  $l$ th ( $l = 1, \dots, L$ ) symbol, the same two memory locations are updated according to:

$$PC_l = PC_{l-1} * \cos(\theta) - PS_{l-1} * \sin(\theta)$$

$$PS_l = PC_{l-1} * \sin(\theta) + PS_{l-1} * \cos(\theta)$$

As required,  $PC_l$  and  $PS_l$  are the phase correction coefficients  $\cos(l*\theta)$  and  $\sin(l*\theta)$ , respectively. The periodic nature of the phase correction coefficients can be further utilized to prevent finite precision errors from accumulating. This is due to the fact that the coefficients generated using the foregoing equations are periodic with a period of  $N/2$  symbols. The period is

$N/2$  as opposed to  $N$  in the illustrated embodiment because the  $f_{off}$  values noted above are even numbers. Thus, when  $l = N/2$ , the memory locations are reset to  $(PC_{N/2}, PS_{N/2}) = (1,0)$ .

In accordance with a further method for generating the coefficients, the receiver may utilize a lookup table. In accordance with this method, the periodic nature of the coefficients is utilized to construct two tables for each window. Each table contains  $N/2$  real numbers corresponding to one of the twin phase correction coefficients required by consecutive symbols. Thus, for eight windows, a total of  $8N$  locations are required. The size of each memory location is contingent on the amount of available memory and necessary mathematical precision. An advantage of using a lookup table procedure is that finite precision errors are completely avoided. Depending on which window is utilized, the corresponding pair of coefficient tables is selected. Starting with the first entry in the table, the receiver simply reads out the phase correction coefficients for the  $l$ th symbol from the  $l$ th row of the two tables in a cyclic manner.

FIGs. 18 and 19 illustrate one manner of modifying the receiver of the RSU 30 so that it may store and process the symbol data for the symbol alignment process. As illustrated, the output of the analog-to-digital converter 190 is concurrently provided to the input of the receiver correlator (FIG. 8) and a RAM block 900. Preferably, only the four most significant bits of the output of the analog-to-digital converter 190 are applied to the RAM block 900.

A preferred implementation of the RAM block 900 is illustrated in FIG.

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19. As shown, a pair of 138 x 4 bit, 2-port RAMs 905 receive data from the analog-to-digital converter 190 and are connected to supply this data to a digital signal processor 910. The read and write operations to and from the RAMs 905 are under the control of a control and address generator circuit 915 and the digital signal processor 910. The data supplied to the digital signal processor 910 is processed in accordance with the operations described above to attain symbol alignment.

Once the receiver 110 has acquired downstream symbol alignment, the system proceeds to step 740 (FIG. 16) where it acquires the downstream communications channel. The downstream communications channel comprises one or more bins used by the head end unit to establish initial communications with receivers 110.

After the receiver 110 has acquired the downstream communications channel, setup of the remote service unit communications proceeds to step 750.

At step 750, the newly added or newly powered-up remote service unit 30 must inform the head end unit 25 that it is in need of registration whereby, among other things, the head end unit 25 allocates bins to the receiver and transmitter of the remote service unit 30. One problem associated with any initial transmission from the remote service unit 30 to the head end unit 25 is that the transmit boundary of the newly added remote service unit is not aligned with the transmit boundary of the other remote service units on the system. Thus, any misaligned transmission from the newly added remote service unit may corrupt the transmissions received from other remote service units.

One way of overcoming the problem of initial misalignment is illustrated in FIG. 20. To overcome the problem, a predetermined upstream bin is allocated as an upstream multi-access channel. The transmitter of the newly added remote service unit transmits information on the upstream multi-access channel in the illustrated manner by altering both its transmit phase and transmit power. As shown, the newly added remote service unit first maintains its transmit phase at a predetermined phase while gradually increasing the transmit power. The head end unit 25 can receive such a signal without a corresponding corruption of the data transmitted from the other remote service units. Once the head end unit 25 detects the transmission from the newly added remote service unit, it can perform any requisite processing of the received signal, such as equalization thereof. After a predetermined period of time has elapsed, the newly added remote service unit begins to slowly vary the phase of its transmitted signal in the illustrated manner. The transmit phase is varied so as to convey intelligent data to the head end unit 25. Accordingly, the head end unit 25 samples the phase of the signal that it receives on the upstream multi-access channel and uses the data, for example, to identify the newly added remote service unit.

After the newly added remote service unit has been identified by the head end unit 25, the head end unit 25 commands the newly added remote service unit, via the downstream communications channel, to send, for example, a broad band, periodic signal. The bandwidth of the transmitted signal should be sufficiently broad so that the signal does not interfere with the

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receipt of transmissions from other remote service units 30 by the head end unit 25. One such broad band signal that may be used is an impulse signal of a predetermined amplitude on the upstream communications channel that is transmitted at the symbol rate. Using the same basic method described above in connection with the remote service unit, the head end unit 25 detects the time position of the impulse signal and provides the remote service unit with the information necessary to align its symbol transmissions with the symbol transmissions of the other remote service units. That is, the head end unit 25 directs the transmitter of the newly added remote service unit 30 to transmit its symbols in alignment with symbol transmissions received from other remote service units. After the head end unit 25 has directed the remote service unit 30 to align its symbol transmissions, the remote service unit 30 discontinues further transmission of the broad band periodic signal. Further communications between the newly added remote service unit and the head end unit 25 can take place on the upstream and downstream communications channels until the head end unit 25 allocates the transmit and receive bins that are to be assigned to the newly added remote service unit and instructs it accordingly. Once the foregoing has been completed, the head end unit 25 and the newly added remote service unit carry out their standard communications at step 760. It should be noted from the foregoing description, that the initialization processes described above take place without interrupting communications between the head end unit 25 and the other remote service units 30 in the system.

FIGs. 21 and 22 illustrate two modifications that may be made to the

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transmitter illustrated in FIG. 10 to add a predetermined signal, such as the above-mentioned impulse signal, to the upstream data to allow the head end unit 25 to determine where in time the transmitter of the remote service unit 30 is transmitting and direct it to transmit in the appropriate upstream time slot. In the embodiment of FIG. 20, an adder 920 is connected to receive the output of register 925 and the output of a sequence ROM or generator circuit 930. The sequence ROM 930 receives sequence sample selection signals along one or more lines 935 provided by the timing and control circuit 940. In response to these signals, the sequence ROM 930 provides digital data values along one or more lines 945 to the input of the adder 920. These digital data values correspond to the predetermined signal, such as the above-noted impulse signal, that is added to one or more symbols of the upstream data transmission or, alternatively, transmitted alone without the transmission of upstream symbols. The timing and control circuit 940 provides the appropriate sequence sample selection signals required to add the predetermined signal at a given periodic rate.

In the embodiment of FIG. 22, an adder/subtractor 950 is connected to receive the output of register 925 and the output of a multiplexer 955. The multiplexer 955 includes two inputs, one input being set to a zero state and the other input being sent to a constant value "k". The multiplexer 955 receives its output selection signal along line 960 provided by the timing and control circuit 940. In response to the output selection signal, the multiplexer 955 provides digital data values corresponding to either the "0" or the constant "k" along one



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or more lines 965 to the input of the adder/subtractor 950 at the appropriate times in the formatted symbol frame. These digital data values correspond to the above-noted impulse signal of amplitude "k" that is either added to or subtracted from one or more symbols of the upstream data transmission. The determination as to whether the constant "k" is added or subtracted is made within the timing and control circuit 940 that provides a selection signal on line 970 to the multiplexer 955 thereby to assign a polarity to the superimposed signal.

Of further note, although not of particular importance to the symbol alignment processes, is the fact that the present system can be designed to transmit and receive either 4 point constellations or 16 point constellations in a given bin depending on the signal-to-noise ratio in the communications system at the bin frequency. This determination is made by the head end unit 25 and the remote service unit(s) transmitting and/or receiving in that bin are instructed accordingly. In bins having a low signal-to-noise ratio, it is preferable to use 4 point constellations. In bins having a high signal-to-noise ratio, it is preferable to use 16 point constellations.

With the foregoing in mind, it can be seen why the embodiments of the remote service units described herein send and receive data in nine bins, respectively. In high noise conditions, four bins are needed by each of the two phones at the customer site to transmit data and four bins are needed by each of the two phones at the customer site to receive data. A total of eight bins are thus required in high noise conditions for each telephone receiver and

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transmitter, respectively. The further ninth bin may, for example, be used to facilitate a bin swapping function.

Although the present invention has been described with reference to specific embodiments, those of skill in the art will recognize that changes may be made thereto without departing from the scope and spirit of the invention as set forth in the appended claims.

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